

Influence of Microstructure on the Interphase Exchange Coupling of $\text{Nd}_2\text{Fe}_{14}\text{B} + 10 \text{ wt}\% \text{Fe}$ Nanocomposites Obtained by Mechanical Milling

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Abstract: The influence of the microstructure on the magnetic interphase exchange coupling of $\text{Nd}_2\text{Fe}_{14}\text{B} + 10 \text{ wt}\% \alpha\text{-Fe}$ nanocomposites obtained through mechanical milling was studied as a function of the milling energy (shock, friction and the ball impact energy) by varying only the size of the grinding media (steel balls with diameters of 5, 10, 15, and 20 mm). The mean crystallite sizes in both $\text{Nd}_2\text{Fe}_{14}\text{B}$ and $\alpha\text{-Fe}$ were studied through X-ray diffraction, by the Scherrer method. The variation in milling energy had little impact on the mean crystallite sizes for $\alpha\text{-Fe}$; approximately 10 nm after annealing at 700 °C for 1.5 min and 20 nm after annealing at 800 °C for 1.5 min. However, after annealing, the $\text{Nd}_2\text{Fe}_{14}\text{B}$ crystallites present average sizes ranging from 50 nm (for the lowest impact energy used) to 20 nm (for high impact energy), with no significant variation due to annealing temperature in the investigate range. Increasing the milling energy does not lower the mean crystallite size beyond 20 nm for the hard magnetic phase. The influence of the microstructure on the magnetic interphase exchange coupling between the hard and soft magnetic phases is reflected in the demagnetization curves and dM/dH vs. H plots for the annealed samples. The samples in which the $\text{Nd}_2\text{Fe}_{14}\text{B}$ phase presents lower mean crystallite sizes show an improvement in both coercivity and energy product over the samples with larger grains. Further improvement in the magnetic interphase coupling can be observed as the average crystallite sizes decrease to 20 nm, for which the highest values for the coercive field $H_c = 0.65 \text{ T}$ and energy product $(\text{BH})_{\text{max}} = 110 \text{ KJ/m}^3$ were recorded.

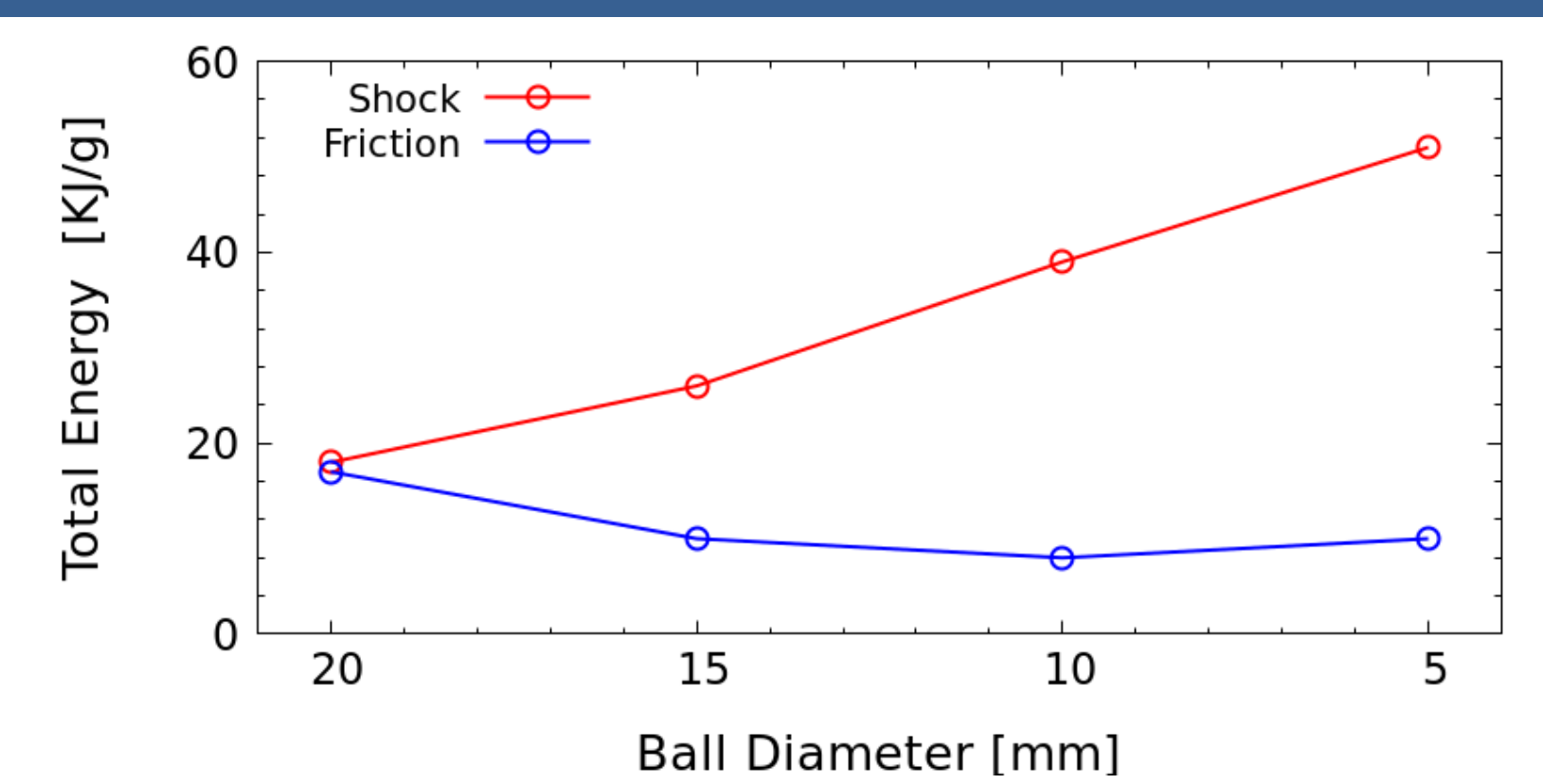
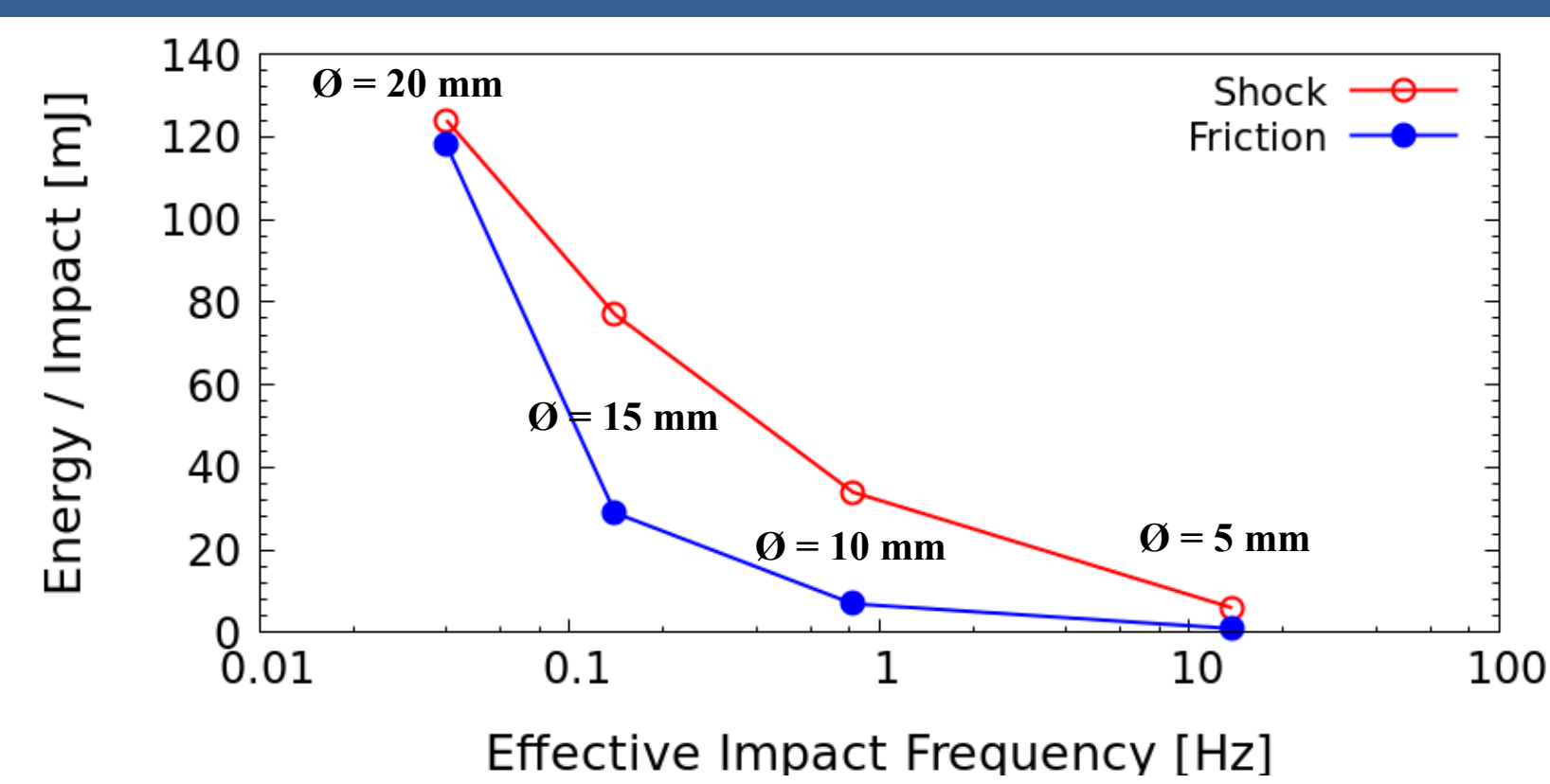
Experimental Details:

- The $\text{Nd}_2\text{Fe}_{14}\text{B}$ phase was prepared : arc melting $\text{Fe}_{14}\text{B} \rightarrow$ induction melting $\text{Fe}_{14}\text{B} + \text{Nd}$ (under purified Ar gas) $\rightarrow$ annealing in vacuum for 72 h at 950 °C. $\rightarrow$ ground to a fine powder under 500 μm .
- The soft magnetic phase consisted of NC 100.24 commercial Fe powder Höganas product.
- Nanocomposite synthesis: starting powder 90wt% $\text{Nd}_2\text{Fe}_{14}\text{B} + 10\text{wt}\% \text{Fe} \rightarrow 6\text{h MM} \rightarrow$ Short Time Annealing 1.5 min
- The milling energies and impact frequencies were calculated by simulating the milling process [1, 2]
- X-Ray diffraction measurements were performed on a Brüker D8 Advance diffractometer using Cu - $K\alpha$ radiation.
- Scanning electron microscopy (SEM) studies were performed on a Hitachi SU8230 device.
- Magnetic measurements were carried out on powder fixed in epoxy resin at 300 K in applied fields up to 10 T.
- Internal Field: demagnetization factor of 1/3

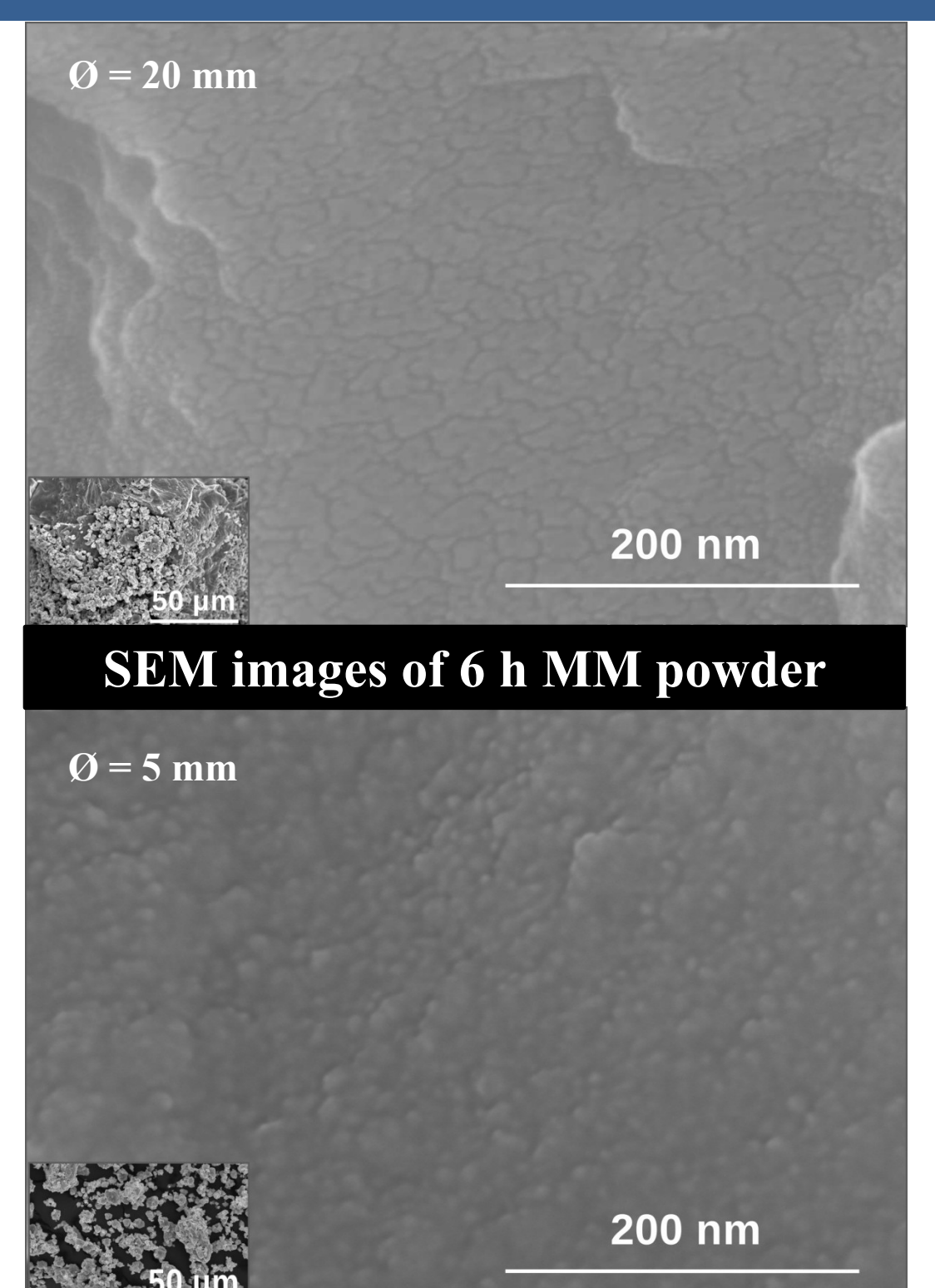
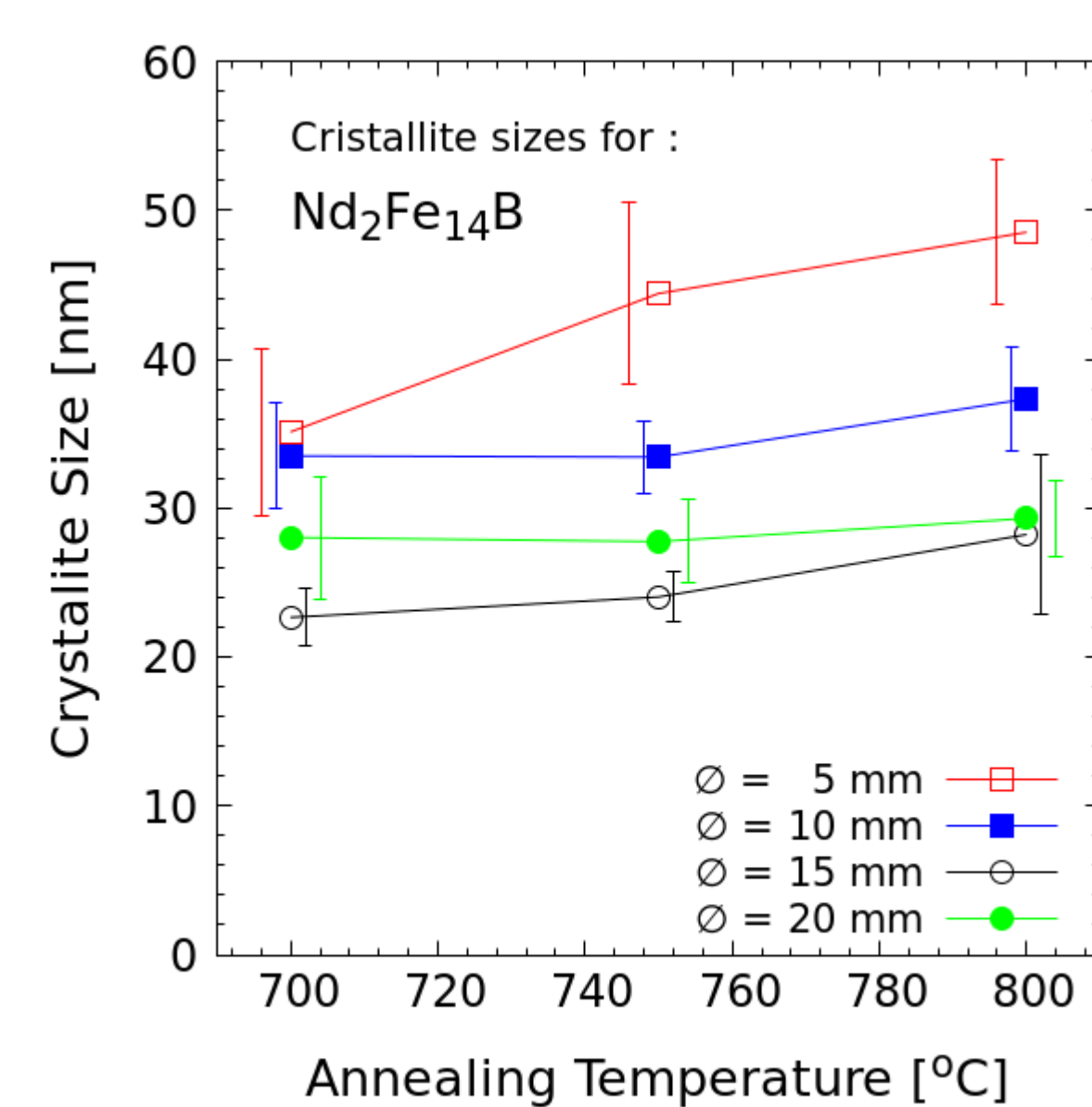
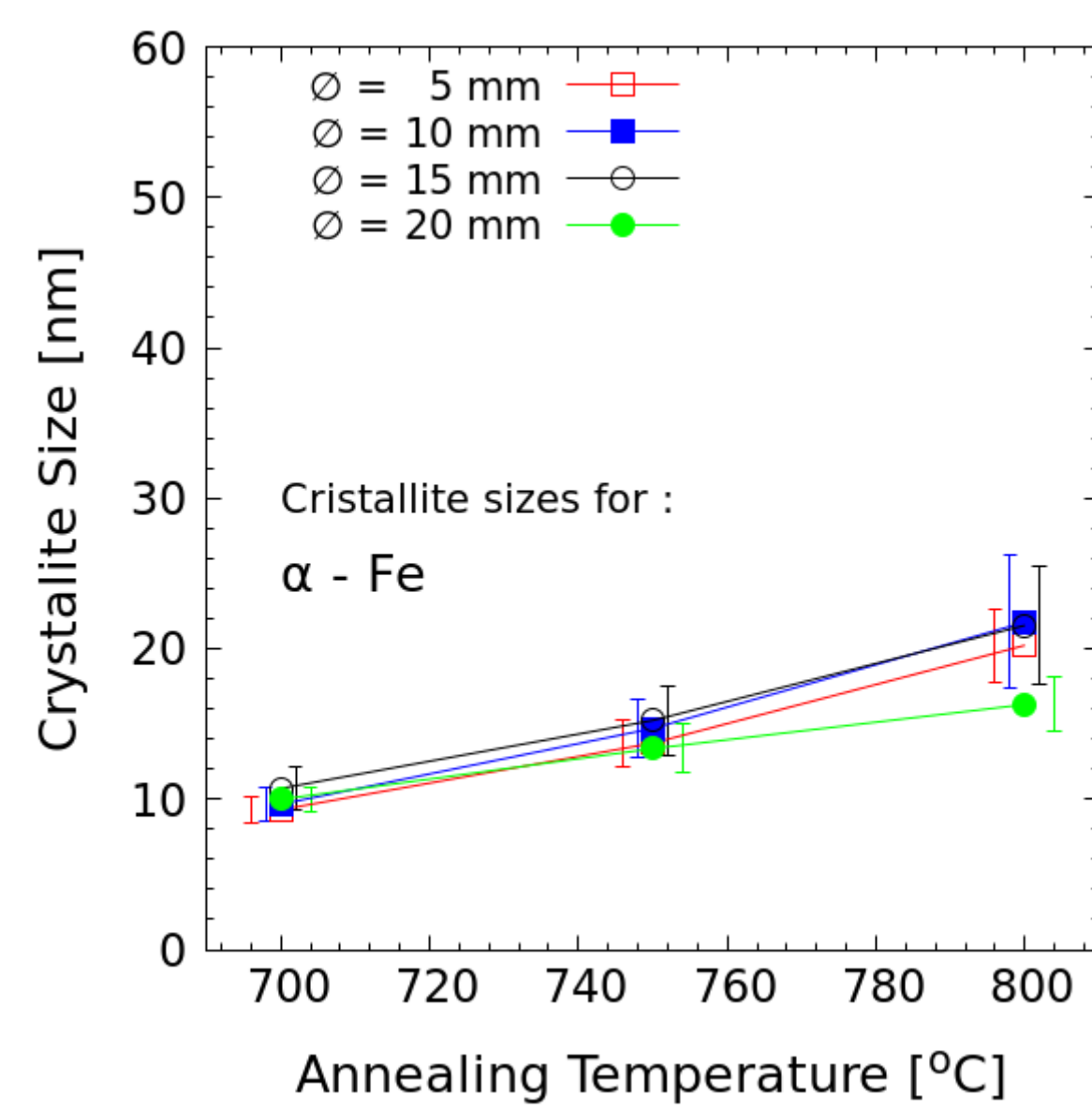
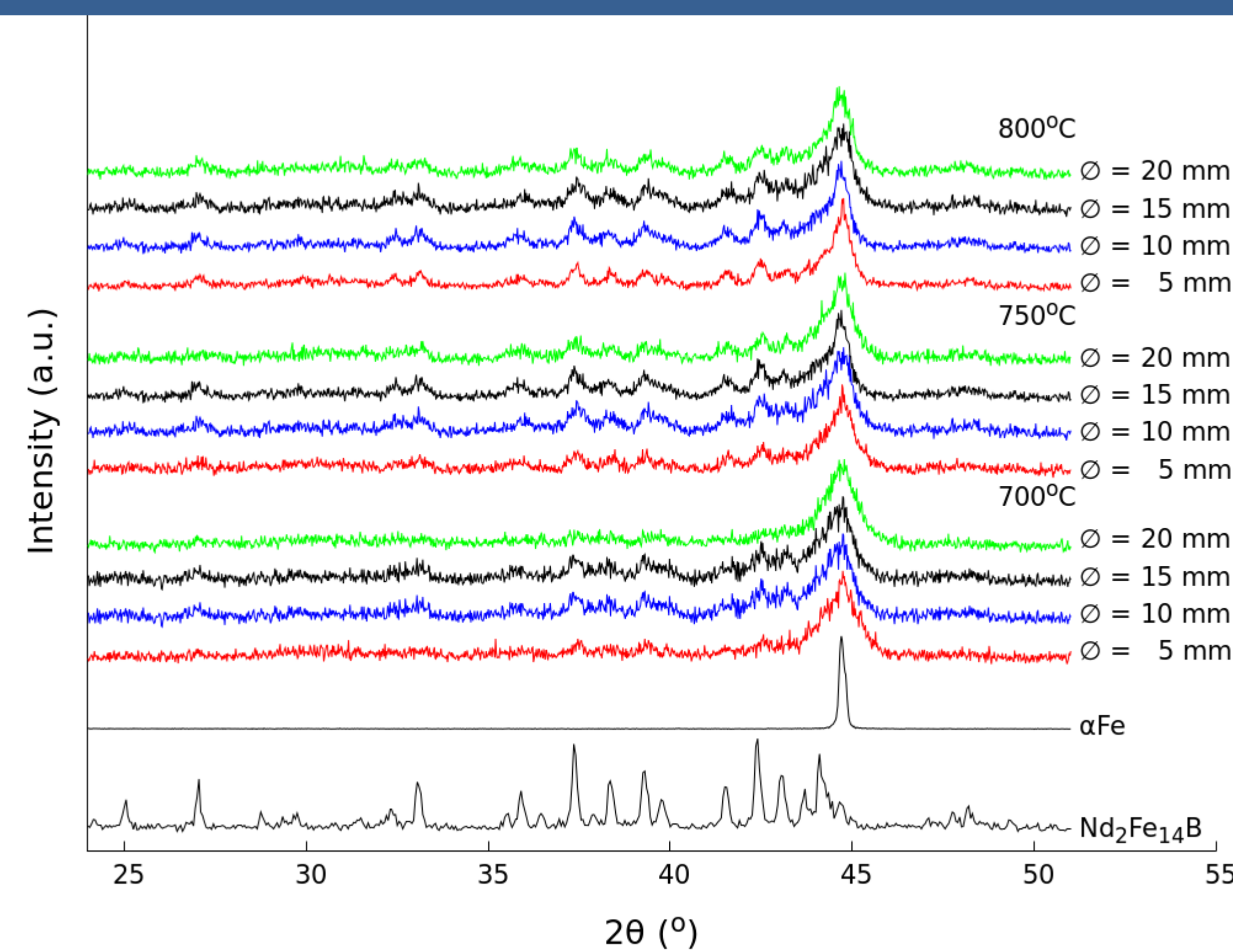
Results and Discussions:

Ball diameter [mm]	Number of Balls
5	209
10	26
15	9
20	4

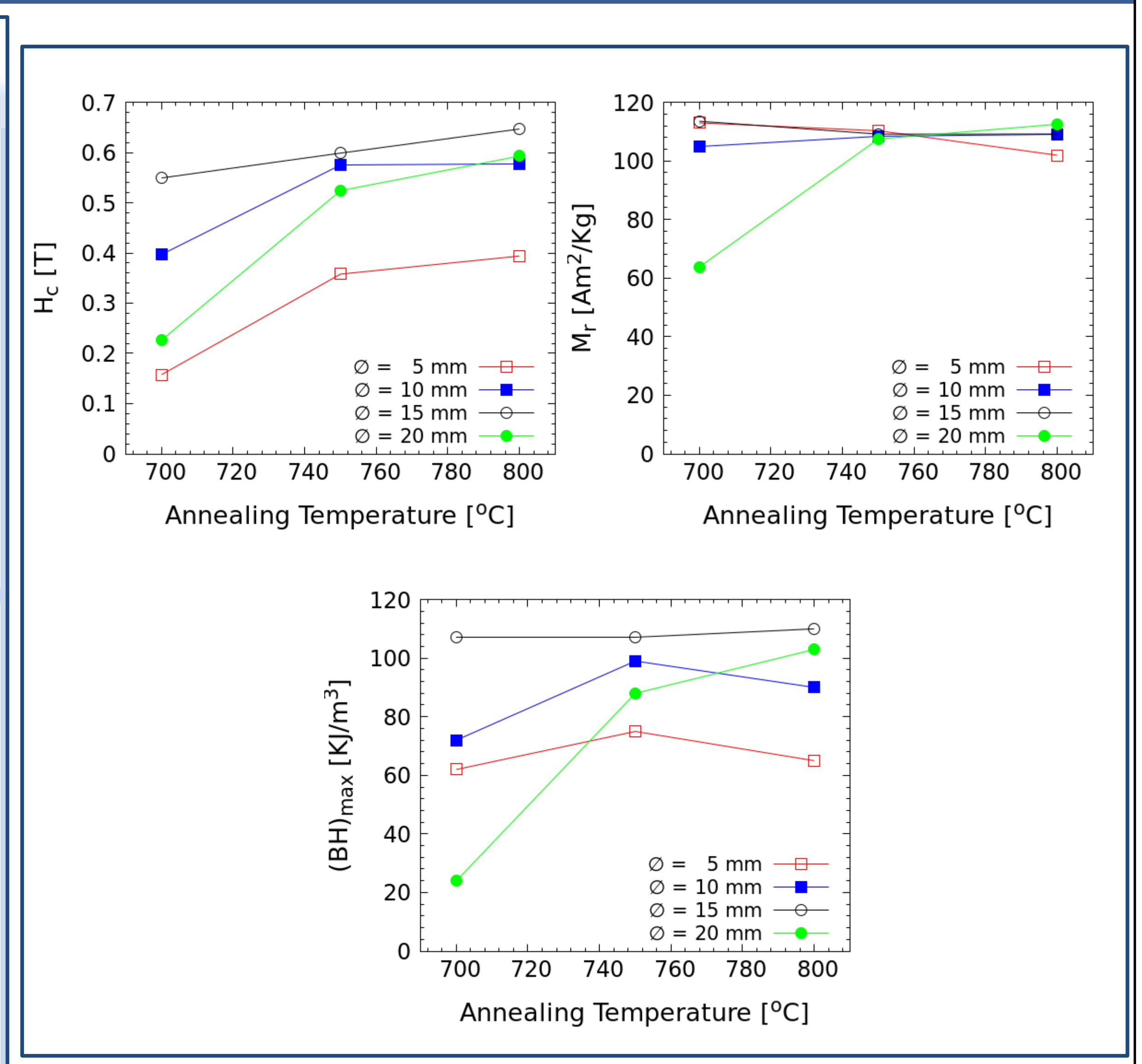
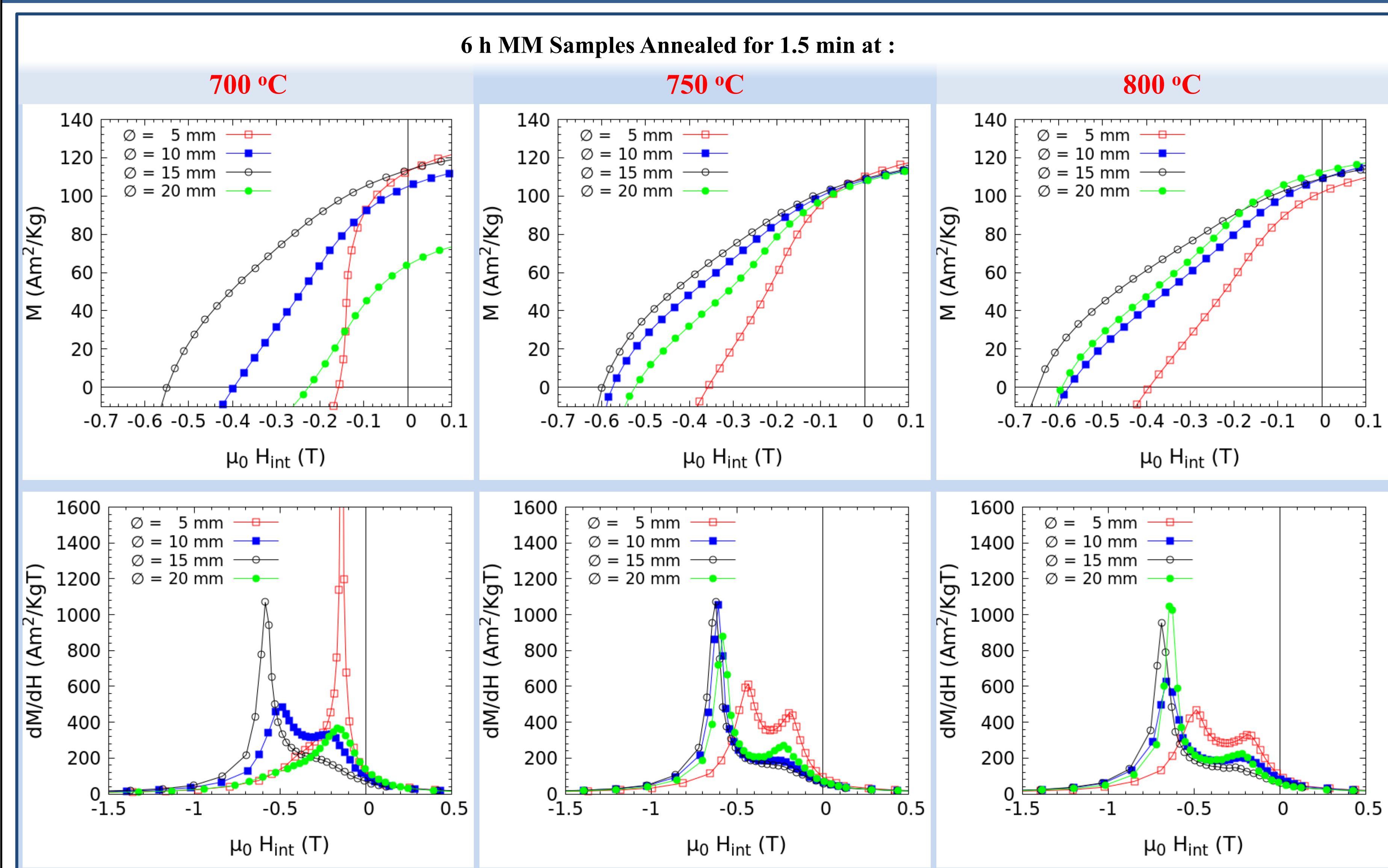
Calculations



Structure and Microstructure



Magnetic Proprieties



Conclusions:

- **Higher impact energy** $\rightarrow$ the **lower $\text{Nd}_2\text{Fe}_{14}\text{B}$ mean crystallite sizes** become (minimum 25 nm).
- **$\alpha\text{-Fe}$ crystallite size** are **affected only by annealing temperature**
- **Smaller $\alpha\text{-Fe}$ and $\text{Nd}_2\text{Fe}_{14}\text{B}$ crystallite sizes** result in a **better interphase exchange coupling** between the hard and soft phase [3]
- **Best results** in the sample set were obtained for the samples **milled with $\varnothing = 15 \text{ mm}$ diameter steel balls and annealed at 800 °C: $H_c = 0.65 \text{ T}$ and $(\text{BH})_{\text{max}} = 110 \text{ KJ/m}^3$**

Acknowledgment

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